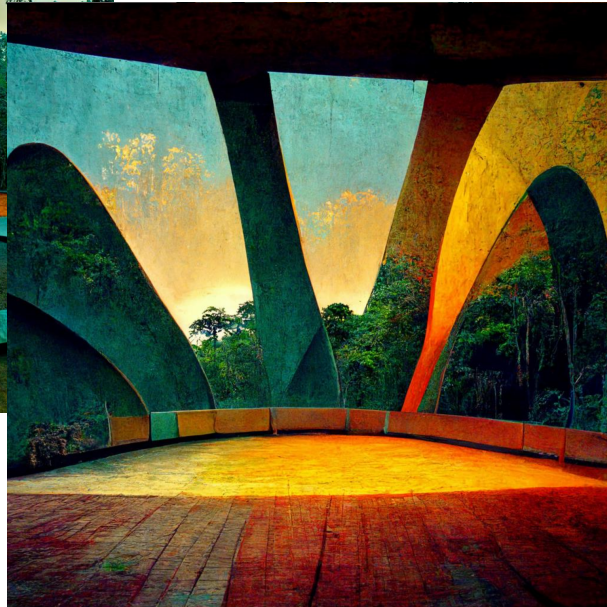


Fall
2022



THTR353

THEATRE DESIGN REPORT
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Introduction

Our proposed theatre, the Davin Stone Demi-Dome (henceforth known as ‘The Dome’), takes inspiration from architectural movements of the 70s, using mostly natural materials and a brown-orange color scheme. Located in the rainforests of Brazil, The Dome can seat over 1600 people, and has a stage over 100 feet wide. The Dome is constructed mainly of locally sourced granite and basalt, as well as a solid mahogany stage. And most importantly, the main feature of the dome is its sloped moss seating, proving ample space for viewing the stage, as well as comfortable, organic seating. The Dome is best suited for large theatre productions and acoustic music shows; however, any event can find a home at The Dome.

Acoustic Treatments

Overview

Since the roof of the theatre is made of basalt, and the floor is covered with moss, the RT60 for high frequencies was too short, while the RT60 for lower frequencies was too long. Heavy treatment of pegboard was needed on the basalt roof of the theatre to bring the RT60 within the target range of ~1.2 seconds. Reflection paths can be seen in Appendix A.

Calculations

Surface area and volume measurements were taken using tools in Rhino3d and can be seen in **Table I**. With over 60000 sq. ft. of moss and around 40000sq. ft. of seatable area, around 5000 people can be comfortably seated with a 9sq. ft. area for each person. Inverse square losses can be calculated using the equation below, along with the distance to the back of the seating in the balcony from center stage, which is about 170ft or 52m.

$$inverse\ square = 20 \log \left(\frac{52m}{1m} \right) = 34.32dB$$

At a spoken level of 74dB, people seated in the back of the theatre would hear 39.68dB from the performer when unamplified, which is extremely quiet.

Once the individual absorption coefficient for each surface was calculated using **Tables I and II**, the full and empty space RT60 values were calculated using the formula below, where V is the volume of the room, S is the surface area of that surface, and a is the absorption coefficient of that surface.

$$RT_{60} = 0.049 * \frac{V}{-S \ln(1 - a)}$$

The RT60 value at each frequency was recorded in **Table III**, and a graph showing the space’s frequency response can be seen in **Fig. 1**. Lastly, the critical distance for the full and empty theatre was calculated at each frequency using the following equation, with V being the volume of the theatre:

$$d_c = 0.014 \sqrt{\frac{V}{RT_{60}}}$$

Table I Room Geometry

Room Faces	Surface Area (ft ²)	Surface Area (m ²)	Coverage %
A (Seating)	60670.82	18491.56	36.70%
B (Stage)	3299.06	1005.50	2.00%
C (Dome)	54241.96	16532.14	32.81%
D (Side Walls)	44094.53	13439.36	26.67%
E (Other Floor)	2999.06	914.07	1.81%
Total	165305.43		

The critical distance at each frequency can be seen in **Table III**.

Table II Absorption Coefficients

Surface Description	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz
Wood, Mahogany	0.19	0.23	0.25	0.3	0.37	0.42
Rock, Basalt	0.05	0.18	0.42	0.64	0.74	0.86
Rock, Granite	0.01	0.01	0.01	0.01	0.02	0.02
Moss	0.01	0.03	0.15	0.35	0.44	0.48
Pegboard - 12.7in centers	0.98	1.1	0.99	0.71	0.4	0.2

Table III RT60 and Critical Distance

Critical Distance (m)	125Hz	250Hz	500Hz	1000Hz	2000Hz	4000Hz
Empty	30.290	33.731	36.676	38.828	37.185	35.927
Full	36.306	40.719	42.479	42.850	40.571	38.682
RT60	125	250	500	1000	2000	4000
Empty	1.900	1.532	1.296	1.156	1.261	1.350
Full	1.322	1.051	0.966	0.949	1.059	1.165

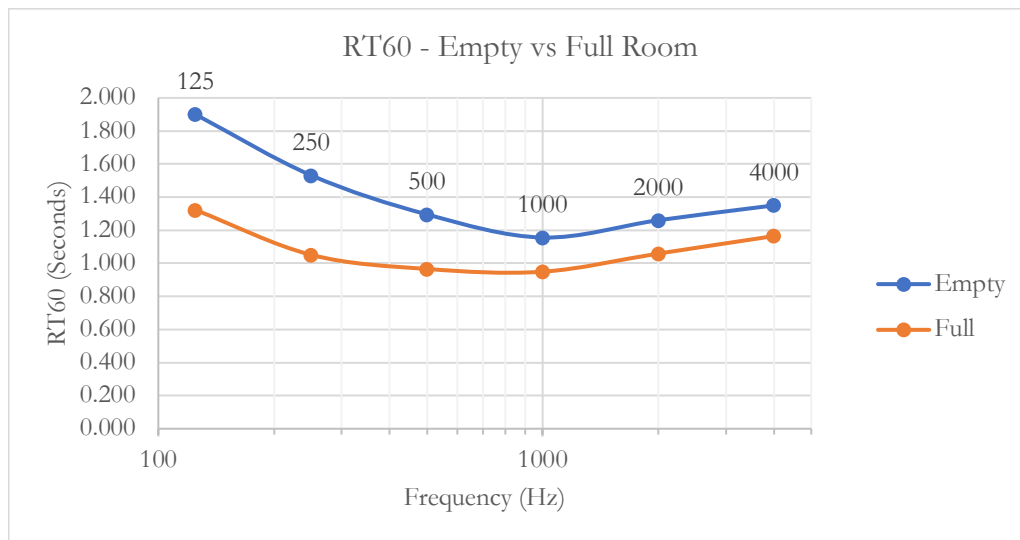


Fig.1. RT60 Curves

Floor Treatments

Over 95% of the floor is covered in moss for seating, while the remaining ~5% is granite. The moss provides mild attenuation of high frequencies, and this dampening is improved further when the theatre is

full. With plenty of space on the ceiling of the theatre for acoustic treatment, further treatment of the floor would needlessly reduce seating capacity.

Ceiling Treatments

The surface of the ceiling receives a 70% treatment of pegboard with 6.4mm holes on 2.5cm centers over 12.7in. Since almost a third of the surface area of the theatre is the roof, the basalt caused the theatre to sound too dead at frequencies above 1kHz. The pegboard treatment counteracts this, simultaneously lowering the RT60 for low frequencies and raising the RT60 for high frequencies into our target range of ~1.2s.

Stage Treatments

The stage makes up only 2% of the surface area of the theatre, and it provides mild absorption across the spectrum, as the stage is mahogany. Ample treatment is provided on the surface of the ceiling, so no further treatment is necessary.

Loudspeaker Design

Overview

The house system is using Meyer's flagship new line array cabinet, Panther. Panther is the ideal array system as it can put out the decibels needed to fill the venue, has 20% less power draw than an average line array cabinet, and allows for pinpoint dispersion control which provides incredible response prediction. In the Davin Demi-Done we have a total of 76 Meyer Panther cabinets; Each of our four main clusters for the orchestra has 10 cabinets while our balcony has 7 cabinets per array. Additionally, spread across the large proscenium we have 8 individual cabinets of Meyer Panthers filling in the gaps. All of this, paired with four arrays of Meyer 900-LFC with a total of 24 cabinets. The block diagram and system connections can be seen in **Appendix B**. This system has an average SPL-C weight of 112dB with a maximum linear peak SPL at 138dB at full strength. This allows the Davin Demi-Done to fit the large shows that come through but can still make a single performer show feel full and vibrant but not overpowering. No external amplifiers are needed as all of Meyer's speakers are active. No sensitivity specification is provided by Meyer for their speakers; however, frequency specifications can be seen in **Table IV**.

Table IV Loudspeaker Specifications

Panther	
Freq. Range	55Hz - 16kHz
Max Sound Level	150.5dB
LFC-900	
Freq. Range	31Hz - 125Hz
Freq. Response	30Hz - 85Hz
Max Sound Level	140dB

With a needed acoustic gain (NAG) of 40.91dB, and a potential acoustic gain (PAG) of 41.27dB after accounting for 6dB of headroom, there is enough room between the PAG and the NAG to reach a level of 85dB in the back of the balcony with a loudspeaker output of 125.91dB.

Calculations

Due to how Meyer Sound handles their speaker specifications, most of our placement and loudspeaker quantities were determined through simulation trial and error. Pictures showing the results of our simulated system can be seen in **Fig.3-5**.

The measurements used in the calculations for PAG and NAG can be seen below in **Fig.2**, along with the equations for PAG and NAG.

$$PAG = 20 \log_{10} \left(\frac{D_1}{D_s} * \frac{D_0}{D_2} \right) = 47.27dB$$

$$PAG \text{ with headroom} = 47.27dB - 6dB = 41.27dB$$

$$NAG = 20 \log_{10}(D_2) = 40.91dB$$

$$\text{desired output} = 85dB$$

$$\text{loudspeaker output} = \text{desired out} + NAG = 125.91dB$$

Table V Potential and Needed Acoustic Gain

Potential/Needed Acoustic Gain	
Ds (ft)	0.167
D0 (ft)	153.133
D1 (ft)	27.94
D2 (ft)	111
PAG (dB)	47.27
PAG w/ FSM(dB)	41.27
NAG (dB)	40.91
Desired Output (dB)	85
Loudspeaker Output (dB)	125.91

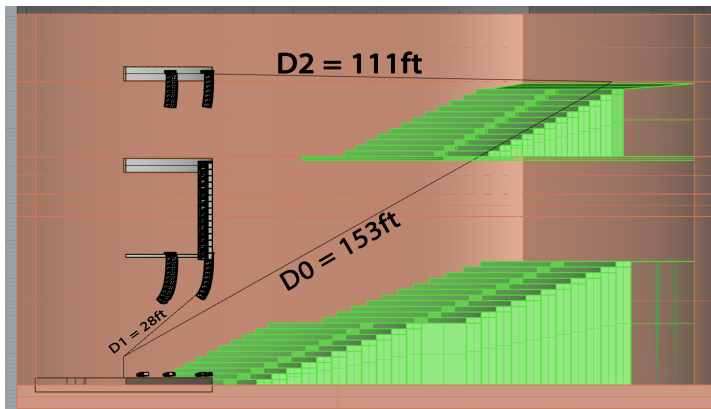


Fig.2. PAGNAG Measurements

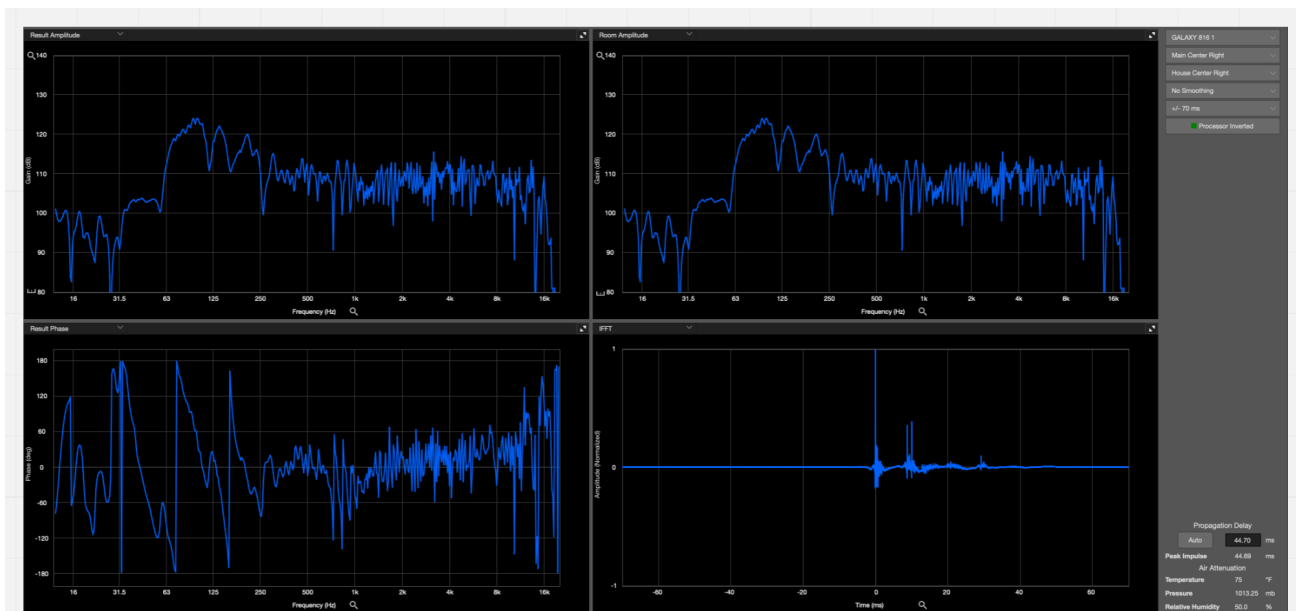


Fig.3. Theatre Sound System Frequency Response

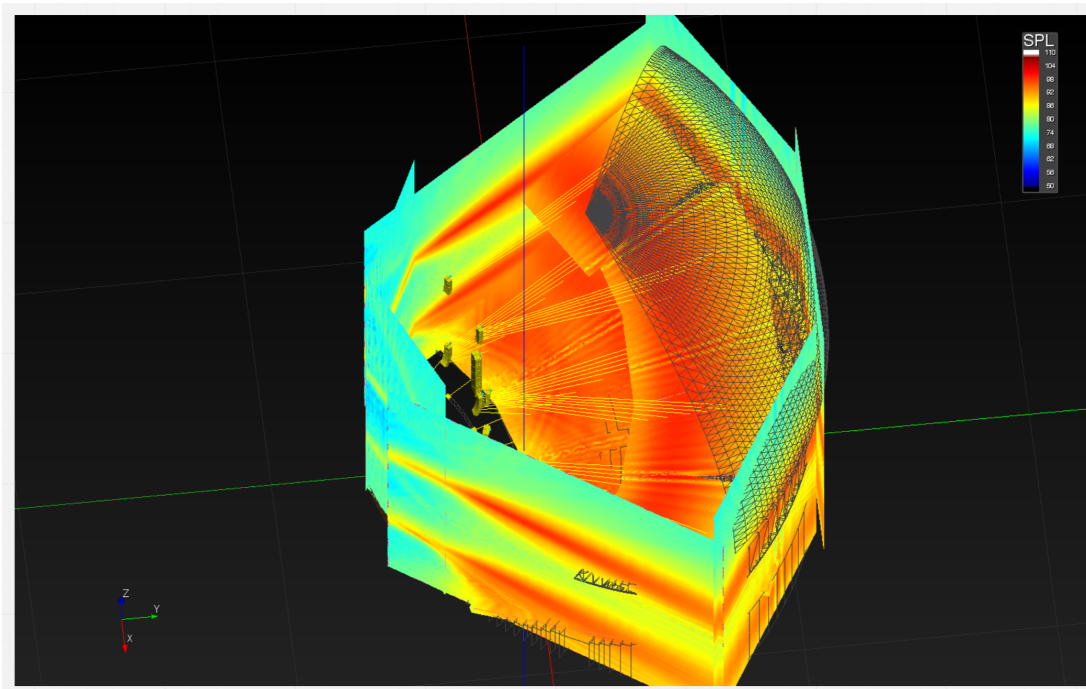


Fig.4. SPL Output at Seating, Side Angle

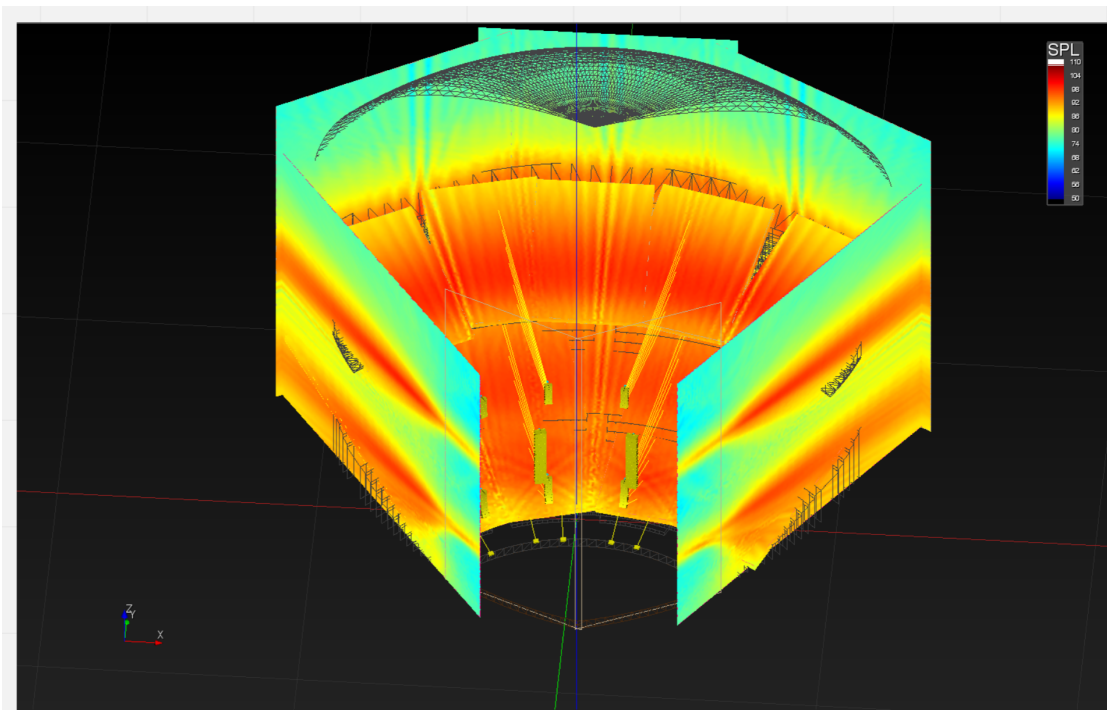


Fig.5. SPL Output at Seating, Front Angle

Networking and Signal Processing

Our system contains 8 Galileo Galaxy 816 Digital Signal Processors with 7 having control over individual line arrays. Our 8th processor is being used as a routing machine with 3 analog inputs and running AVB outputs all hitting an Extreme 440 8 port switch which gives signal to the other processors. The processor settings can be seen below in **Appendix C** in **Fig. 14 - Fig. 20**. While setting up our processor we needed to find delay times to accurately time our system for the ideal audience listen experience. Using this equation, we found that our top boxes of Meyer Panther in our balcony arrays has a delay time of 70.4ms. Going down from there, the bottom box has a delay time of 64ms. The position we calculated from was the center stage position which can be seen in **Fig. 7**. Although this system is very big, using Meyer’s equipment, we have been able to simplify the system in a way that allows for easy control, easy access to equipment, and have great user interfaces. A full system schematic can be seen down below in **Appendix B**.

$$Delay\ in\ ms = \frac{Distance\ in\ feet}{1.126}$$

Mixing Console

Appendix A – Room Drawings

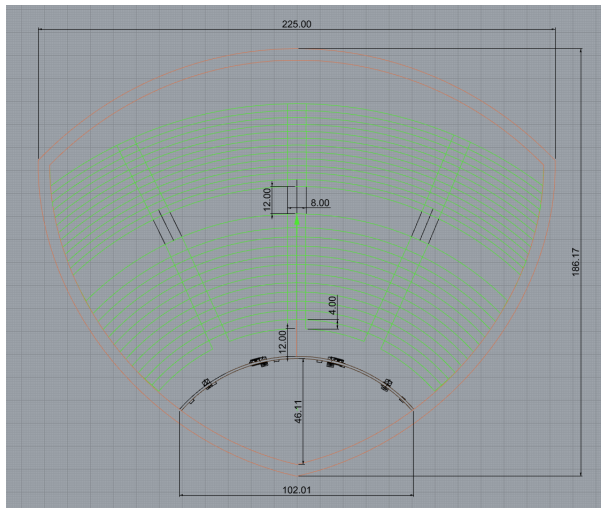


Fig. 6. Annotated Plan (All measurements in feet)

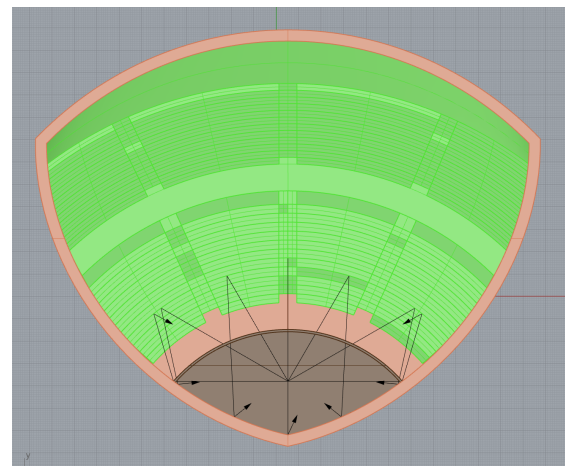


Fig. 7. Plan with Reflections, 30 degrees apart, 2 bounces each

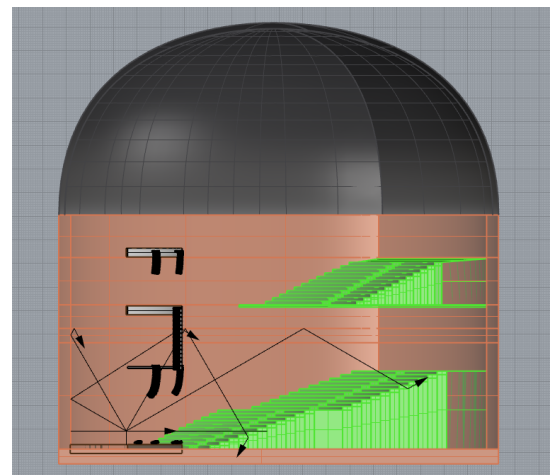
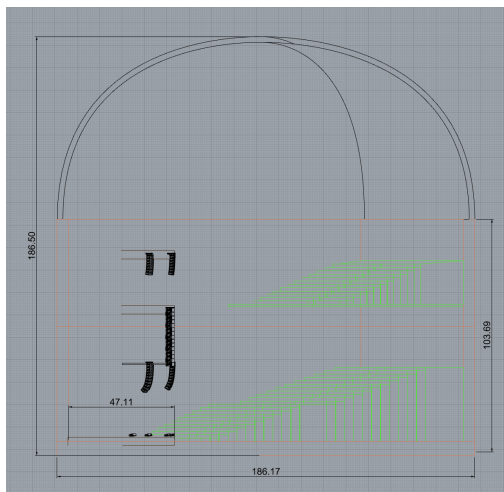


Fig. 9. Section with Reflections, 30 degrees

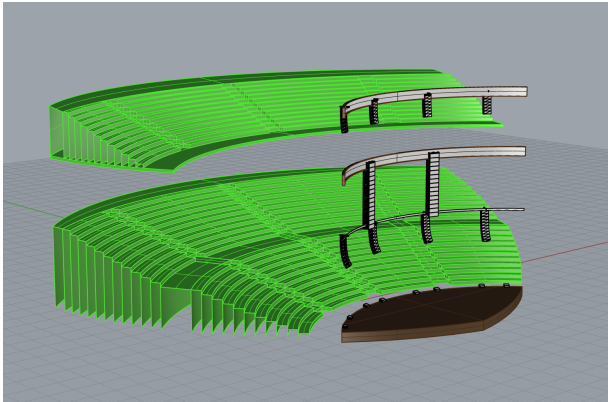


Fig. 10. Stage and seating

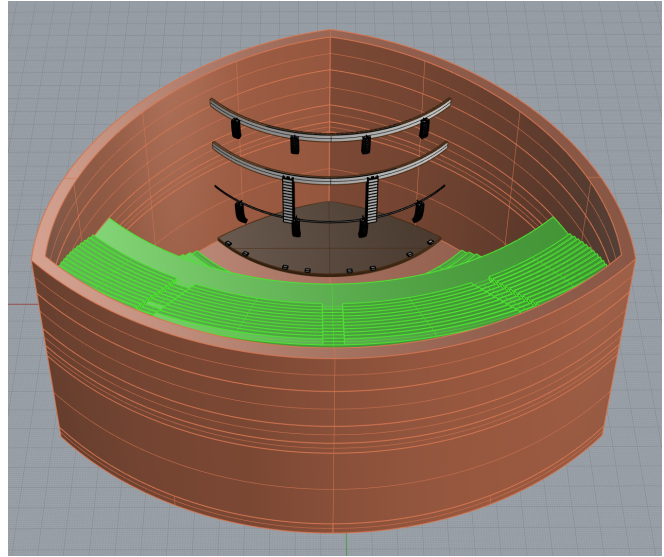


Fig. 11. Back angle of theatre

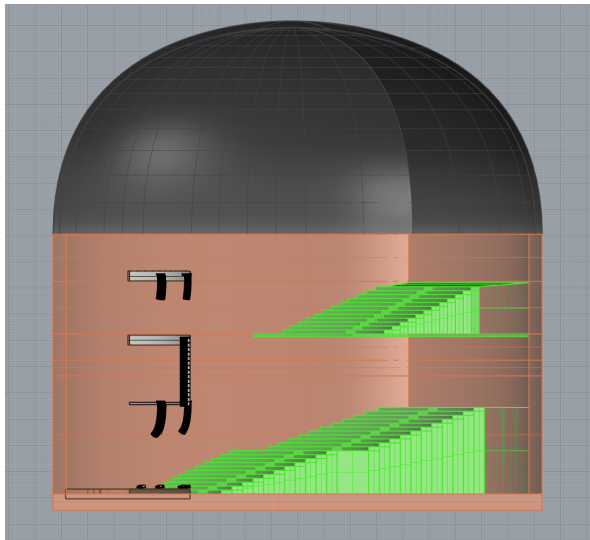


Fig. 12. Half of theatre

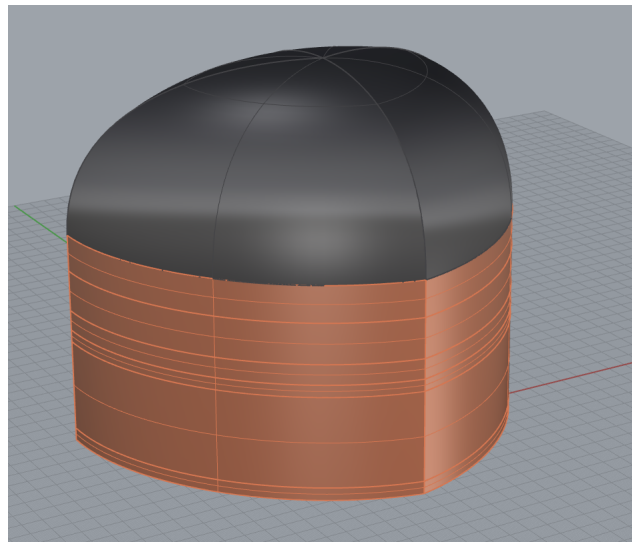
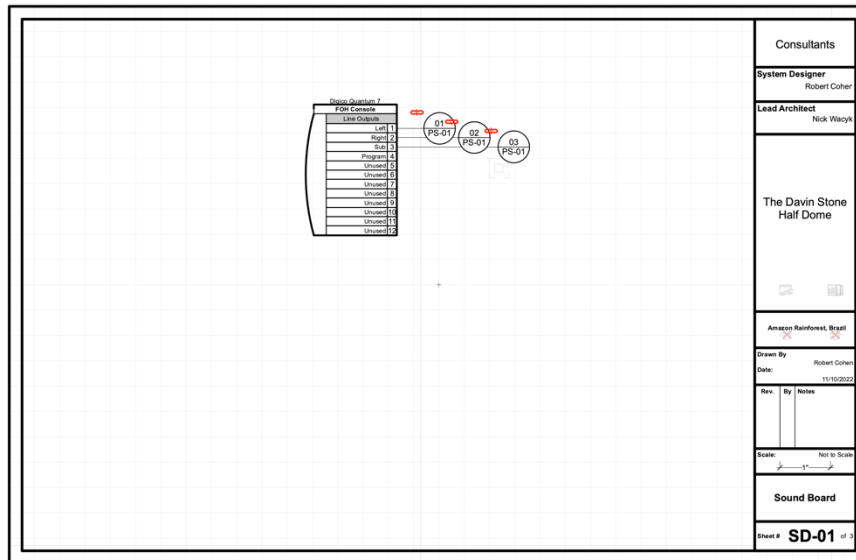


Fig. 13. Fully enclosed dome

Appendix B - System Diagrams



Consultants

System Designer
Robert Cohen

Lead Architect
Nick Wacyk

The Davin Stone Half Dome

Amazon Rainforest, Brazil

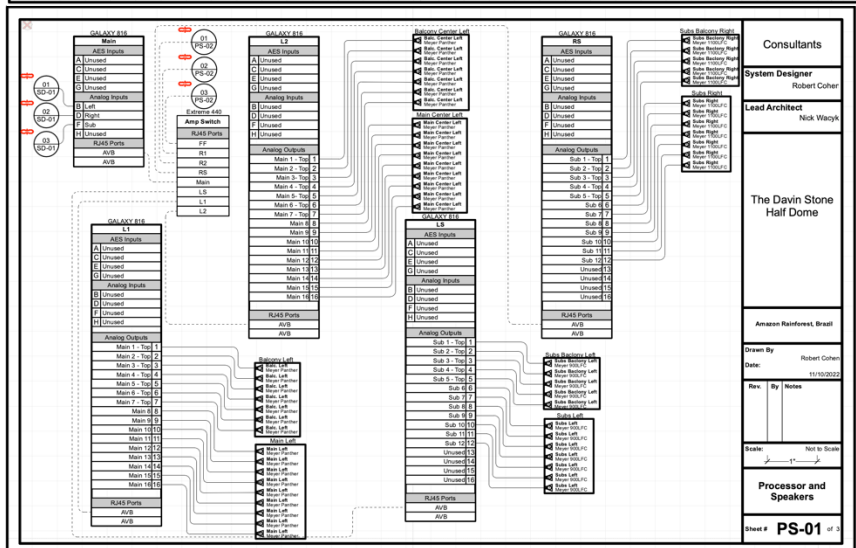
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Date: 11/10/2022

Rev. By Notes

Scale: Not to Scale

Sound Board

Sheet # **SD-01** of 3



Consultants

System Designer
Robert Cohen

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The Davin Stone Half Dome

Amazon Rainforest, Brazil

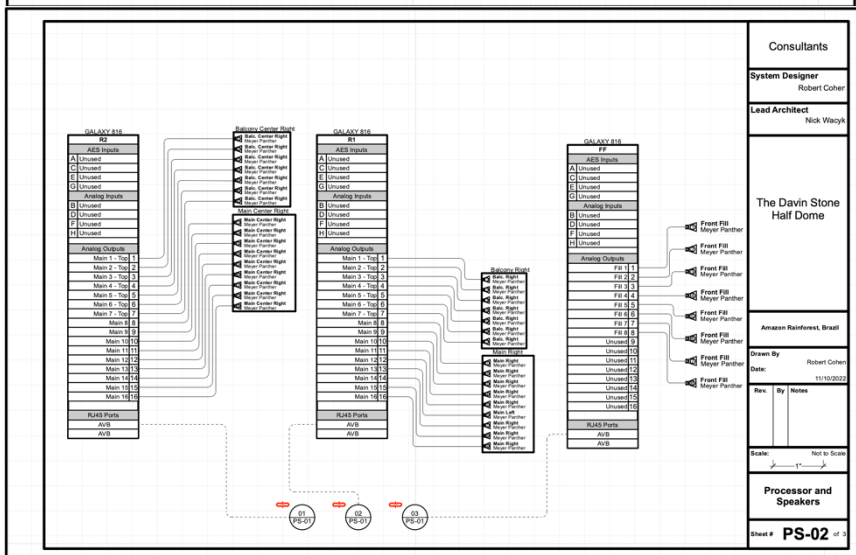
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Rev. By Notes

Scale: Not to Scale

Processor and Speakers

Sheet # **PS-01** of 3



Consultants

System Designer
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Lead Architect
Nick Wacyk

The Davin Stone Half Dome

Amazon Rainforest, Brazil

Drawn By: Robert Cohen
Date: 11/10/2022

Rev. By Notes

Scale: Not to Scale

Processor and Speakers

Sheet # **PS-02** of 3

Appendix C - Processor Settings

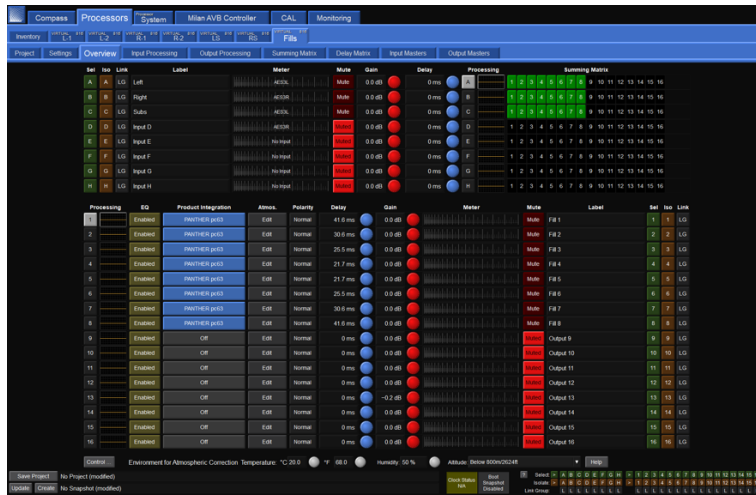


Fig. 14. Front Fills



Fig. 15. Line Arrays Left 1



Fig. 16. Line Arrays Left 2

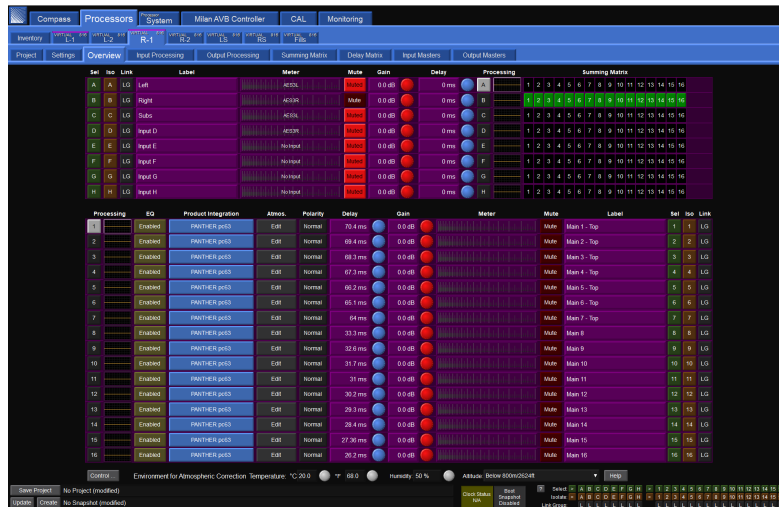


Fig. 17. Line Arrays Right 1



Fig. 18. Line Arrays Right 2

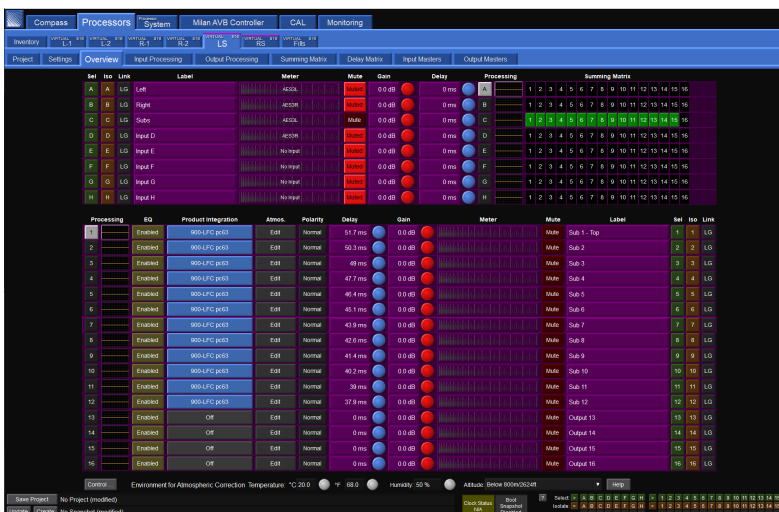


Fig. 19. Line Arrays Subs Left

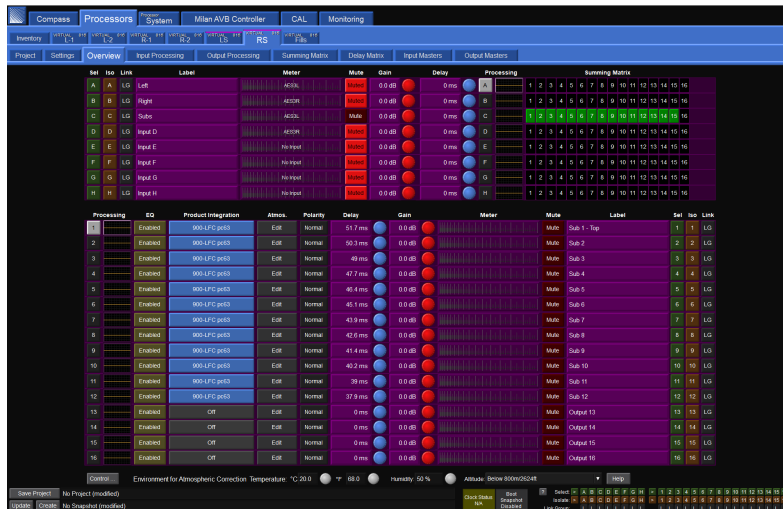


Fig. 20. Line Arrays Subs Right